

# Influence of $\beta$ Nucleation Agent on the Dispersion of Nano-CaCO<sub>3</sub> in Isotactic Polypropylene Matrix

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**ABSTRACT:** To study the interaction between  $\beta$ -nucleation agent and nano-CaCO<sub>3</sub> in iPP matrix, the dynamic rheology properties, crystallization and melting behaviors, impact fracture surface of  $\beta$ -nucleation agent ( $\beta$ -NA) nucleated and nano-CaCO<sub>3</sub> filled iPP were investigated in details in this study. Under suitable conditions, the  $\beta$ -NA has a "promoting dispersion effect" on the dispersion of nano-CaCO<sub>3</sub> in PP matrix. However, 0.2 wt %  $\beta$ -NA nucleated sample has a worse "promoting dispersion effect" than 0.05 wt %  $\beta$ -NA nucleated sample at relatively high nano-CaCO<sub>3</sub> content (7.5 wt %). The reason is that 0.2 wt %  $\beta$ -NA aggregates on the surface of nano-CaCO<sub>3</sub> agglomerations. The  $\alpha$  crystals induced from  $\beta$ -crystals grow more regular and perfect than conventional  $\alpha$  crystals. For the relative fraction of  $\beta$  crystals ( $K_{\beta}$ ), the nano-CaCO<sub>3</sub> content has little influence on 0.05 wt %  $\beta$ -NA nucleated samples, but obvious effect on 0.2 wt %  $\beta$ -NA nucleated samples. Based on the investigated results, a mechanism model about the interaction between  $\beta$ -nucleation agent and nano-CaCO<sub>3</sub> in iPP matrix is proposed. © 2012 Wiley Periodicals, Inc. J. Appl. Polym. Sci. 000-000, 2012

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#### INTRODUCTION

Isotactic polypropylene (iPP) is one of the most important thermoplastic polymers due to its low cost and excellent properties.<sup>1</sup> It has four modifications:  $\alpha$ ,  $\beta$ ,  $\gamma$ , and smectic,<sup>2–5</sup> among them the  $\beta$ -form is the most attractive one for its better impact resistance as well as higher heat distortion temperature than other forms.<sup>6,7</sup> The  $\beta$ -form is metastable thermodynamically and can be obtained under some special conditions, such as in the presence of specific heterogeneous nucleation agents,<sup>8-10</sup> by crystallization in a temperature gradient during processing,<sup>11,12</sup> or by shear-induced crystallization.<sup>13–15</sup> Adding  $\beta$ -nucleation agent is the most effective and accessible method to get a high level of  $\beta$ -PP.<sup>16</sup> However, the yield strength and stiffness of iPP parts is lowered by the presence of  $\beta$  crystals.<sup>17,18</sup> It has been speculated that adding some inorganic fillers, such as calcium carbonate, to  $\beta$ -crystals-rich matrix is a potential way to achieve a stiffness-impact balance of PP.19

Labour et al.<sup>20,21</sup> investigated the influence of the  $\beta$  crystalline phase caused by specific temperature gradient on the mechanical properties of unfilled and CaCO<sub>3</sub>-filled polypropylene and found that 0.1–1  $\mu$ m CaCO<sub>3</sub> particle size is the most optimum for stopping cracks. Kotek et al.<sup>22</sup> explored the tensile properties of isotactic polypropylene modified by specific nucleation and active fillers (CaCO<sub>3</sub>), and discovered that the combination of specific  $\beta$ -nucleation and inorganic fillers can lead to materials with higher ductility and higher modulus than neat isotactic polypropylene. Mai et al.<sup>7,23</sup> proposed a way for producing a novel highly efficient  $\beta$ -NA for polypropylene using nano-CaCO<sub>3</sub> as a support, and found that the crystallization and melting temperatures as well as the content of  $\beta$  phase in iPP nucleated using the supported  $\beta$ -nucleator are higher than those of iPP nucleated using traditional  $\beta$ -nucleator.

Nevertheless, to the best of our knowledge, there are few studies concerning the interaction between  $\beta$  nucleation agent and nano-CaCO<sub>3</sub> in the matrix. In the present work, the interaction between  $\beta$  nucleation agent (TMB-5) and nano-CaCO<sub>3</sub> particles in isotactic polypropylene matrix was investigated in details using dynamic rheology test, DSC investigation, SEM observation. Based on the investigated results, a mechanism model about the interaction between  $\beta$ -nucleation agent and nano-CaCO<sub>3</sub> in iPP matrix is proposed.

## EXPERIMENT

## Materials

A commercial grade of iPP (T30S) was supplied by Lanzhou Petrochemical Company, China, with a melt flow index (MFI)

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Materials

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Table I.	Formula	of PP/Nano-	-CaCO <sub>3</sub> / $\beta$ -NA	Composites	Prepared	via	Melt
Compo	unding						

Sample abbreviation	Nano-CaCO <sub>3</sub> content (wt %)	β-NA content (wt %)
PP/0/0	0	0
PP/0/0.05	0	0.05
PP/0/0.2	0	0.2
PP/2.5/0	2.5	0
PP/2.5/0.05	2.5	0.05
PP/2.5/0.2	2.5	0.2
PP/5/0	5	0
PP/5/0.05	5	0.05
PP/5/0.2	5	0.2
PP/7.5/0	7.5	0
PP/7.5/0.05	7.5	0.05
PP/7.5/0.2	7.5	0.2

of 2.6 g/10 min (230°C/2.16 kg) and a density of 0.91 g cm<sup>-3</sup>, respectively. The  $\beta$ -nucleation agent ( $\beta$ -NA, TMB-5) is aryl amide-based system and was provided by Fine Chemicals Department of Shanxi Provincial Institute of Chemical Industry, with a melting temperature of 348.9°C. The nano-calcium carbonate, with an average particle size of 15–30 nm, was purchased from Shanxi Haize Nano-materials and it was pretreated with stearic acid.

The designed composites formula is depicted in Table I.

#### **Sample Preparation**

A two-step process was employed to prepare the composites. TMB-5 was first melt mixed with pure iPP to form masterbatch containing 5 wt %  $\beta$ -NA. Then, the master-batch was compounded with pure iPP and nano-CaCO<sub>3</sub> using a SHJ-25 twin-screw extruder. The screw speed was fixed at 120 rpm, and the processing temperature profile was limited within 135– 200°C from hopper to die.

The mixed pellets were then injection molded into a rectangular parallelopiped shape by a PS40E5ASE injection molding machine with a barrel temperature of 205°C, mold temperature of 60°C and injection pressure of 35 MPa.

For preparing dynamic rheology tests, the mixed pellets were compression molded into specific disks (1.2-mm thick with a diameter of 25 mm) at 200°C for 5 min. The applied pressure was 10 kN. The force was released to zero twice to allow any potential gas to escape.

#### Characterization

**Dynamic Rheology Tests.** Dynamic rheology properties were investigated using a rotational rheometer (Malvern Instruments, Bohlin Gemini 200). Steady shear measurement was performed at the shear rate of  $0.01-100 \text{ s}^{-1}$  at  $200^{\circ}$ C.

**DSC Tests.** The crystallization and melting behaviors of the samples were carried out on a TA Q200 differential scanning calorimeter in a nitrogen atmosphere. A sample about 8 mg was first heated up to 200°C and held on for 5 min to release ther-

mal history. Then, it was cooled down to  $40^{\circ}$ C at a cooling rate of  $10^{\circ}$ C min<sup>-1</sup> to investigate the crystallization behavior of the sample. After maintaining at  $40^{\circ}$ C for 1 min, it was heated up again to  $200^{\circ}$ C at  $10^{\circ}$ C min<sup>-1</sup> to explore the melting behavior of the sample.

The fusion enthalpy  $(\Delta H_i)$  of  $\alpha$  crystal and  $\beta$  crystals was obtained by the methods proposed by Li,<sup>24</sup> and the crystallinities of the  $\alpha$ - and  $\beta$ -phase were calculated separately according to equation:

$$X_i = \Delta H_i / (\Delta H_i^0 \times \Phi c) \times 100\%$$
(1)

where  $\Delta H_i$  is the calibrated specific fusion heat of either the  $\alpha$ -phase or the  $\beta$ -phase,  $\Delta H_i^0$  is the standard fusion heat of either  $\alpha$ -phase or the  $\beta$ -phase crystals, 178 J g<sup>-1</sup> for the former and 170 J g<sup>-1</sup> for the latter, and  $\Phi_c$  is the weight percentage of iPP in composites. The relative fraction of  $\beta$ -phase ( $K_\beta$ ) in the matrix can be calculated from the following equation:

$$K_{\beta} = \frac{X_{c\beta}(\%)}{X_{c\alpha}(\%) + X_{c\beta}(\%)} \times 100\%$$
<sup>(2)</sup>

where  $X_{c\alpha}$  (%) and  $X_{c\beta}$  (%) are the degrees of crystallinity for  $\alpha$ -phase and  $\beta$ -phase, respectively.

**SEM Observation.** Impact fracture surface of the composites was observed using a Hitachi scanning electron microscope (S4800). The surface was coated with gold prior to the observation and the SEM was operated at 5.0 kV.

#### **RESULTS AND DISCUSSION**

#### **Dynamic Rheology Analysis**

Dynamic rheology test is a good way to investigate the dispersion of fillers in the composites melt. Figure 1 shows the effect of nano-CaCO3 content on the complex viscosity of nonnucleated sample, 0.05 wt %  $\beta$ -NA nucleated sample and 0.2 wt %  $\beta$ -NA nucleated sample, respectively. It can be seen that the composites exhibit non-Newtonian (shear thinning) behavior at all shear rate ranges. In Figure 1(a), complex viscosity increases with nano-CaCO<sub>3</sub> content at first (PP/2.5/0 and PP/5/0), but decreases when the content reaches 7.5 wt % in non-nucleated sample. It indicates that 2.5 and 5 wt % nano-CaCO3 can disperse well in non-nucleated matrix, while there exists many agglomerations in PP/7.5/0 sample. However, as shown in Figure 1(b), 7.5 wt % nano-CaCO<sub>3</sub> filled PP (PP/7.5/0.05) has a higher complex viscosity than 2.5 and 5 wt % nano-CaCO<sub>3</sub> filled PP, which reflects that better dispersion of nano-CaCO<sub>3</sub> particles can be achieved by the incorporation of  $\beta$ -NA. One possible reason for this phenomenon is that the  $\beta$ -NA particles have some effective interaction with nano-CaCO<sub>3</sub> particles, which has lowered its surface energy, thus leading to a relative good dispersion of nano-CaCO3 particles. Nevertheless, the PP/ 7.5/0.2 sample exhibits similar viscosity to PP/5/0.2 and PP/2.5/ 0.2 sample, as shown in Figure 1(c). It indicates that 0.2 wt %  $\beta$ -NA nucleated sample has a worse "promoting dispersion effect" than 0.05 wt %  $\beta$ -NA nucleated sample at relatively high nano-CaCO<sub>3</sub> content (7.5 wt %).



**Figure 1.** Effect of nano-CaCO<sub>3</sub> content on the complex viscosity of (a) non-nucleated sample, (b) 0.05 wt %  $\beta$ -NA nucleated sample and (c) 0.2 wt %  $\beta$ -NA nucleated sample, respectively. [Color figure can be viewed in the online issue, which is available at wileyonlinelibrary.com.]

Figure 2(a) shows the effect of  $\beta$ -NA on the rheology behavior of nonfilled sample. The addition of  $\beta$ -NA has lowered the viscosity of composites, and it's more obvious for PP/0/0.05 than PP/0/0.2. It suggests that  $\beta$ -NA, as small molecules, can diminish the viscosity of melt, acting like a lubricant. However, 0.2 wt %  $\beta$ -NA tends to aggregate, which is detrimental to the lubricant effect. As exhibited in Figure 2(b)no obvious difference can be seen for 2.5 wt % nano-CaCO3 filled sample with various  $\beta$ -NA content, for the reason that 2.5 wt % nano-CaCO<sub>3</sub> tends to disperse well in the matrix, the "promoting dispersion effect" of  $\beta$ -NA has little influence on it. Figure 2(c) presents the effect of  $\beta$ -NA on the complex viscosity of 7.5 wt % nano-CaCO<sub>3</sub> filled sample. The  $\beta$ -NA tends to accumulate at a concentration of 0.2 wt %, which limits its "promoting dispersion effect" in the matrix. As a result, 0.2 wt % nucleated sample has a lower viscosity than 0.05 wt %  $\beta$ -NA nucleated sample and a higher viscosity than non- $\beta$ -NA-nucleated sample when the nano-CaCO<sub>3</sub> content is 7.5 wt %.

#### **DSC Results Analysis**

**Crystallization Behavior.** Figure 3 depicts the crystallization temperature of composites of various  $\beta$ -NA contents and nano-CaCO<sub>3</sub> contents. It can be seen that nano-CaCO<sub>3</sub> has less effect on crystallization temperature than  $\beta$ -NA, indicating that  $\beta$ -NA content is the key factor for determining crystallization temperature. For non- $\beta$ -NA-nucleated and 0.05 wt %  $\beta$ -NA nucleated sample, the crystallization temperature increases a little with the addition of nano-CaCO<sub>3</sub>, while the crystallization temperature of 0.2 wt %  $\beta$ -NA nucleated sample keeps almost constant. There are two reasons to explain this phenomenon: first, 0.05 wt %  $\beta$ -NA is not saturated for nucleation, while 0.2 wt %  $\beta$ -NA tends to reach the saturated state; second, there may exist a specific intrinsic construction weakening the nucleation ability of nano-CaCO<sub>3</sub> in 0.2 wt %  $\beta$ -NA nucleated sample.

**Melting Behavior.** Figure 4(a) shows the effect of nano-CaCO<sub>3</sub> content on the melting behavior of non- $\beta$ -NA-nucleated sample.

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**Figure 2.** Effect of  $\beta$ -NA content on the complex viscosities of (a) non-filled sample, (b) 2.5 wt % nano-CaCO<sub>3</sub> filled sample and (c) 7.5 wt % nano-CaCO<sub>3</sub> filled sample, respectively. [Color figure can be viewed in the online issue, which is available at wileyonlinelibrary.com.]

With increasing the nano-CaCO<sub>3</sub> content, the crystallinity increases from 53.56% (PP/0/0) to 55.41% (PP/7.5/0). Besides, there exists a tiny  $\beta$  crystals melting peak in PP/7.5/0 sample, while not in other three samples. It has been reported that nano-CaCO<sub>3</sub> is a kind of  $\beta$  nucleation agents by some researchers.<sup>25,26</sup>

Figure 4(b) depicts the effect of nano-CaCO<sub>3</sub> content on the melting behavior of 0.05 wt %  $\beta$ -NA nucleated sample. One can observe that there are two  $\alpha$  melting peaks in some samples, one lies in 161–163°C region (low  $\alpha$  melting peak), the other one lies in 167–168°C region (high  $\alpha$  melting peak). In Figure 4(a)the  $\alpha$  melting peak lies in 161–163°C region. With the addition of 0.05 wt %  $\beta$ -NA, the high  $\alpha$  melting peak appears. It can be attributed to that some  $\alpha$  nuclei grows on  $\beta$  crystals in a specific temperature gradient that has been reported by some researchers.<sup>21</sup> The  $\alpha$  crystals initiated by

these nuclei grow more regular and perfect than conventional  $\alpha$  crystals. There is only the high  $\alpha$  melting peak in PP/0/0.05, for the reason that the majority of  $\alpha$  crystals are induced by  $\beta$  crystals, indicating a fine dispersion of 0.05 wt %  $\beta$ -NA. With the addition of nano-CaCO<sub>3</sub>, the low  $\alpha$  melting peak emerges. It can be explained that the dispersion of  $\beta$ -NA in nano-CaCO<sub>3</sub> filled samples is somewhat different, some "conventional"  $\alpha$  crystals come into being in some "without- $\beta$ -NA" region.

Figure 4(c) presents the effect of nano-CaCO<sub>3</sub> content on the melting behavior of 0.2 wt %  $\beta$ -NA nucleated sample. There are two  $\alpha$  melting peaks in samples PP/0/0.2. It indicates that 0.2 wt %  $\beta$ -NA can not disperse well in the composites. But as the nano-CaCO<sub>3</sub> content increases to 7.5 wt %, only the low  $\alpha$  melting peak exists. The possible reason is that the dispersion of 0.2 wt %  $\beta$ -NA in PP/7.5/0.2 is relatively bad, there is more

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**Figure 3.** The crystallization temperature of composites of various  $\beta$ -NA contents and nano-CaCO<sub>3</sub> contents. [Color figure can be viewed in the online issue, which is available at wileyonlinelibrary.com.]



**Figure 4.** Effect of nano-CaCO<sub>3</sub> content on the melting behavior of (a) non-nucleated sample, (b) 0.05 wt %  $\beta$ -NA nucleated sample and (c) 0.2 wt %  $\beta$ -NA nucleated sample, respectively. [Color figure can be viewed in the online issue, which is available at wileyonlinelibrary.com.]



**Figure 5.** The relative fraction of  $\beta$  crystals ( $K_{\beta}$ ) of 0.05 and 0.2 wt %  $\beta$ -NA nucleated with the addition of nano-CaCO<sub>3</sub>. [Color figure can be viewed in the online issue, which is available at wileyonlinelibrary.com.]

"blank" region in composites to promote the growth of "conventional"  $\boldsymbol{\alpha}$  crystals.

The relative fraction of  $\beta$  crystals ( $K_{\beta}$ ) of 0.05 and 0.2 wt %  $\beta$ -NA nucleated with the addition of nano-CaCO<sub>3</sub> is shown in Figure 5. No obvious difference can be found between non-filled and 2.5 wt % nano-CaCO<sub>3</sub> filled samples for the reason that 0.05 wt %  $\beta$ -NA can disperse well in the matrix, so the nano-CaCO<sub>3</sub> has little influence on it. As the nano-CaCO<sub>3</sub> concentration increases to 5 or 7.5 wt %, the  $K_{\beta}$  of 0.2 wt %  $\beta$ -NA decreases gradually, while that of 0.05 wt %  $\beta$ -NA keeps nearly unchanged. It indicates that the nucleation ability of 0.2 wt %  $\beta$ -NA is weakened by the incorporation of nano-CaCO<sub>3</sub>.

# SEM Observation

Figure 6 shows the impact fracture surface of various samples. It can be seen from Figure 6(a) that the fracture surface of sample PP/0/0 is relatively smooth, indicative of a brittle behavior. Comparatively, the fracture surface of PP/0/0.05 and PP/0/0.2 is relatively rough, as shown in Figure 6(b, c)which suggests that the incorporation of  $\beta$ -NA can lead to ductile behavior. It can also be observed that some small dots exist in Figure 6(b, c)which may be due to the agglomerations of  $\beta$ -NA. As exhibited in Figure 6(d)there are many nano-CaCO<sub>3</sub> agglomerations in the fracture surface, hinting bad dispersion of nano-CaCO<sub>3</sub> in the composites when the concentration reaches 7.5 wt %. However, the addition of  $\beta$ -NA has promoted the dispersing of nano-CaCO<sub>3</sub>, as displayed in Figure 6(e, f).

## MECHANISM MODEL

Based on the aforementioned investigated results, a mechanism model about the interaction between  $\beta$ -nucleation agent and nano-CaCO<sub>3</sub> in PP matrix is proposed, which is exhibited in Figure 7. With the increment of nano-CaCO<sub>3</sub> in non- $\beta$ -NAnucleated samples, the nano-CaCO<sub>3</sub> particles tend to aggregate (described in Section 3.1), and its average agglomeration size

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Figure 6. Impact fracture surface of (a) PP/0/0, (b) PP/0/0.05, (c) PP/0/0.2, (d) PP/7.5/0. (e) PP/7.5/0.05, and (f) PP/7.5/0.2, respectively.

become larger, as shown in Figure 7(b, c). For the non-filled sample, 0.05 wt %  $\beta$ -NA can disperse well, leading to a homogeneous structure. However, 0.2 wt %  $\beta$ -NA particles can't keep a fine dispersion in the matrix, as proposed by Varga,<sup>27</sup> and the particles have a tendency to form agglomerations, which is exhibited in Figure 7(g). When the nano-CaCO<sub>3</sub> concentration is 2.5 wt %, no clear distinction can be observed among PP/2.5/0, PP/2.5/0.05 and PP/2.5/0.2 for the reason

that 2.5 wt % nano-CaCO<sub>3</sub> can disperse well in the matrix by itself, which has been deducted from dynamic rheology analysis. Under such circumstance, even the  $\beta$ -NA particles are attached to the surface of nano-CaCO<sub>3</sub>, the  $\beta$ -NA has little influence on its dispersion. Thus, the rheology behavior vary little among PP/2.5/0, PP/2.5/0.05, and PP/2.5/0.2. For PP/7.5/ 0.05, the nano-CaCO<sub>3</sub> particles have a intensive tendency to aggregate, but the role of attached  $\beta$ -NA is to lower the surface



Figure 7. The schematic diagram of the mechanism model about the interaction between  $\beta$ -nucleation agent and nano-CaCO<sub>3</sub> in PP matrix. (Circles without hatching lines stand for  $\beta$ -nucleation agent, while the circles with hatching lines mean nano-CaCO<sub>3</sub> particles or agglomerations.)

energy of nano-CaCO<sub>3</sub> particles, so they can disperse better than PP/7.5/0, which has been deducted from Figure 1(a). However, 0.2 wt %  $\beta$ -NA particles are easy to gather together, too, so its "promoting dispersion effect" is weakened. Accordingly, the dispersion of nano-CaCO<sub>3</sub> of PP/7.5/0.2 is not so well as that of PP/7.5/0.05. Although the nano-CaCO3 content increases from 2.5 wt % (PP/2.5/0.2) to 7.5 wt % (PP/7.5/0.2), the total aggregates surface area of PP/7.5/0.05 is larger than that of PP/7.5/0.2 due to the particles agglomeration of the latter. As a result, the  $\beta$ -NA aggregate on the surface of nano-CaCO<sub>3</sub> agglomeration, thus some  $\beta$ -NA is covered so that its  $\beta$ -nucleation effect is influenced, which is presented in Figure 5.

#### CONCLUSIONS

The dynamic rheology properties, crystallization and melting behaviors, impact fracture surface of  $\beta$ -nucleation agent nucleated and nano-CaCO<sub>3</sub> filled PP were investigated, to study the interaction between  $\beta$ -nucleation agent and nano-CaCO<sub>3</sub> in iPP matrix. Some interesting results can be obtained:

Under suitable conditions, the  $\beta$ -NA has a "promoting dispersion effect" on the dispersion of nano-CaCO<sub>3</sub> in PP matrix. However, 0.2 wt %  $\beta$ -NA nucleated sample has a worse "promoting dispersion effect" than 0.05 wt %  $\beta$ -NA nucleated sample at relatively high nano-CaCO<sub>3</sub> content (7.5 wt %). The reason is that 0.2 wt %  $\beta$ -NA aggregates on the surface of nano-CaCO<sub>3</sub> particles. The  $\alpha$  crystals induced from  $\beta$ -crystals grow more regular and perfect than conventional  $\alpha$  crystals. For the relative fraction of  $\beta$  crystals ( $K_{\beta}$ ), the nano-CaCO<sub>3</sub> content has little influence on 0.05 wt %  $\beta$ -NA nucleated samples, but obvious effect on 0.2 wt %  $\beta$ -NA nucleated samples.

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